

# D5.7. Report on reactor and shielding C/E validation and nuclear data trends

Linked to WP5/T5.2/ST5.2.2 – C/E validation and trends

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## 1. Introduction



- Objective: C/E validation to contribute to the improvement of JEFF nuclear data files
- JEFF-based C/E biases are analyzed to identify needs for nuclear data improvement
  - **1.** Reactor physics experiments:
    - 1. IRPhE
    - 2. Partner's own databases: CEA/DES LWR
    - 3. Other legacy experiments: SEFOR, Almaraz NPP (IAEA)
  - 2. Shielding benchmarks: SINBAD

Experiments from different facilities, neutron spectra, and integral quantities of interest



- Different validation strategies applied, all of them based on calculating C/E
- But differing in how they use C/E ratios to assess the quality of the library and identify needs for ND improvement

Mean bias or	Perturbation	Trending analysis	Bayesian-based
weighted mean bias	analysis		analysis
<ul> <li>Different metrics applied</li> </ul>	<ul> <li>Impact of ND perturbations with respect to data from other libraries</li> </ul>	<ul> <li>Comparisons with trending parameters</li> </ul>	• GLLS method



#### Reactor physics benchmarks useful for ND validation (of SFR) have been identified and C/E assessed (UPM) Multiplication factor: set of experiments from IRPhE (12 experiments) with a high similarity to SFR

Benchmark identifier in IRPhEP	Fuel/Other	Experimental facility	Institution
EBR2-LMFR-RESR-001	$\mathrm{UO}_2/Sodium$	EBR-II	ANL, USA
SNEAK-LMFR-EXP-001	MOX/Sodium	SNEAK 7A	KFK, Germany
ZEBRA-LMFR-EXP-001	$\mathrm{Pu}$ metal- $\mathrm{UO}_2/Sodium$	ZEBRA 22	AEEW, UK
ZPPR-LMFR-EXP-001	MOX/Sodium	ZPPR-10A	ANL, USA
ZPPR-LMFR-EXP-002	MOX/Sodium	ZPPR-9	ANL, USA
ZPPR-LMFR-EXP-010	MOX/Sodium	ZPPR-12	ANL, USA
ZPPR-LMFR-EXP-011	MOX/Sodium	ZPPR-2	ANL, USA
ZPR-FUND-EXP-006	Pu-U alloys/Graphite	ZPR-3/53	ANL, USA
ZPR-FUND-EXP-007	Pu-U alloys/Graphite	ZPR-3/54	ANL, USA
ZPR-FUND-EXP-014	Pu-U carbide/Sodium	ZPR-9/31	ANL, USA
ZPR-LMFR-EXP-001	MOX/Sodium	ZPR-6/7	ANL, USA
ZPR-LMFR-EXP-002	MOX/Sodium	ZPR-6/7	ANL, USA





#### Perturbation with NDaST and GLLS for biases analysis

SLIDE 5



#### Sodium void reactivity effect: IRPhE (5 experiments selected)

Benchmark identifier	Experimental facility	Core Loading
ZPPR-LMFR-EXP-010-m12030	ZPPR-12	Loading 30
ZPPR-LMFR-EXP-010-m12033	ZPPR-12	Loading 33
ZPPR-LMFR-EXP-010-m12037	ZPPR-12	Loading 37
ZPPR-LMFR-EXP-011-case08	ZPPR-2	Loading 184
ZPPR-LMFR-EXP-011-case09	ZPPR-2	Loading 185





## Doppler reactivity effect: lack of experiments in IRPhE; SEFOR experiments from SFR-UAM Reflector worth: potential of SEFOR calibration curves for ND validation of <sup>239</sup>Pu, <sup>56</sup>Fe, <sup>58</sup>Ni



	Calculated at UPM					
SEFUR	SCALE-6.2.3 (R-Z model)					
Core II	JEFF-3.1.1	JEFF-3.3	Corrected JEFF-3.3			
Doppler constant	-676.6	-708.9	-688.7			
Core II C/E	1.010	1.058	1.028			





#### U-238 (n,γ) ratio JEFF-3.3/JEFF-3.1.1



his allowed to identify a typo for the 808 eV p-wave  $\Gamma_\gamma$  parameter

#### **4.1 Thermal Reactor Physics benchmarks from IRPHE**

• UPM analyzed C/E in KRITZ benchmarks (LWR lattices at KRITZ reactor in Studsvik) and trends with T<sup>a</sup>



JEFF-3.3, the trend with temperature becomes stronger

Perturbation analysis using NDaST showed biases probably due to  $^{235}$ U(n,fission) ~ 0.01 eV – 1eV

**Ref.:** Kodeli et al. Analysis of the KRITZ Critical Benchmark Experiments, NENE2009



	Cycle 1	Cycle 2	Cycle 3		Cycle 1	Cycle 2	Cycle 3		Cycle 1	Cycle 2	Cycle 3
REL2005	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]	<b>REL2005</b>	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]	REL2005	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]	(C/E-1) ± ∆E/E [%]
<sup>234</sup> U/ <sup>238</sup> U	1.0 ± 0.3	1.2 ± 0.4	1.4 ± 0.5	<sup>234</sup> U/ <sup>238</sup> U	1.1 ± 0.3	1.4 ± 0.4	1.7 ± 0.5	<sup>234</sup> U/ <sup>238</sup> U	1.1 ± 0.3	1.4 ± 0.4	1.6 ± 0.5
<sup>235</sup> U/ <sup>238</sup> U	0.3 ± 0.4	1.3 ± 0.7	1.6 ± 1.3	<sup>235</sup> U/ <sup>238</sup> U	-0.2 ± 0.4	0.1 ± 0.7	-1.0 ± 1.3	<sup>235</sup> U/ <sup>238</sup> U	-0.2 ± 0.4	0.1 ± 0.7	-0.9 ± 1.3
<sup>236</sup> U/ <sup>238</sup> U	0.0 ± 0.2	0.5 ± 0.2	0.3 ± 0.2	<sup>236</sup> U/ <sup>238</sup> U	0.1 ± 0.2	0.7 ± 0.2	0.5 ± 0.2	<sup>236</sup> U/ <sup>238</sup> U	0.1 ± 0.2	0.6 ± 0.2	0.4 ± 0.2
<sup>237</sup> Np/ <sup>238</sup> U	-7.7 ± 2.9	-3.3 ± 2.9	-2.0 ± 2.0	<sup>237</sup> Np/ <sup>238</sup> U	-6.5 ± 2.9	-2.4 ± 2.9	-0.7 ± 2.0	<sup>237</sup> Np/ <sup>238</sup> U	-6.7 ± 2.9	-2.7 ± 2.9	-1.1 ± 2.0
<sup>238</sup> Pu/ <sup>238</sup> U	-5.6 ± 1.9	-4.0 ± 2.0	-3.4 ± 1.8	<sup>238</sup> Pu/ <sup>238</sup> U	-3.6 ± 1.9	-0.3 ± 2.0	3.7 ± 1.8	<sup>238</sup> Pu/ <sup>238</sup> U	-6.2 ± 1.9	-4.5 ± 2.0	-3.4 ± 1.8
<sup>239</sup> Pu/ <sup>238</sup> U	0.6 ± 0.7	0.7 ± 0.9	2.2 ± 1.2	<sup>239</sup> Pu/ <sup>238</sup> U	0.5 ± 0.7	-0.5 ± 0.9	0.5 ± 1.2	<sup>239</sup> Pu/ <sup>238</sup> U	0.7 ± 0.7	0.0 ± 0.9	1.3 ± 1.2
<sup>240</sup> Pu/ <sup>238</sup> U	-1.3 ± 1.2	0.3 ± 0.9	0.5 ± 0.7	<sup>240</sup> Pu/ <sup>238</sup> U	-0.5 ± 1.2	0.6 ± 0.9	1.1 ± 0.7	<sup>240</sup> Pu/ <sup>238</sup> U	-2.2 ± 1.2	-1.3 ± 0.9	-0.9 ± 0.7
<sup>241</sup> Pu/ <sup>238</sup> U	-2.5 ± 2.1	-1.6 ± 1.4	0.0 ± 2.0	<sup>241</sup> Pu/ <sup>238</sup> U	-2.1 ± 2.1	-1.5 ± 1.4	0.0 ± 2.0	<sup>241</sup> Pu/ <sup>238</sup> U	-2.5 ± 2.1	-1.8 ± 1.4	0.0 ± 2.0
<sup>242</sup> Pu/ <sup>238</sup> U	-2.5 ± 3.3	-0.8 ± 2.1	-0.2 ± 1.6	<sup>242</sup> Pu/ <sup>238</sup> U	-2.6 ± 3.3	-0.8 ± 2.1	0.6 ± 1.6	<sup>242</sup> Pu/ <sup>238</sup> U	-3.7 ± 3.3	-2.0 ± 2.1	-0.9 ± 1.6
<sup>241</sup> Am/ <sup>238</sup> U	•	•	-0.1 ± 3.2	<sup>241</sup> Am/ <sup>238</sup> U	•	•	-1.2 ± 3.2	<sup>241</sup> Am/ <sup>238</sup> U	•	•	-1.1 ± 3.2
<sup>241</sup> Am/ <sup>238</sup> U EOC			± 5.4	<sup>241</sup> Am/ <sup>238</sup> U EOC			± 5.4	<sup>241</sup> Am/ <sup>238</sup> U EOC			± 5.4
<sup>242m</sup> Am/ <sup>238</sup> U		211L	8.9 ± 7.0	<sup>242m</sup> Am/ <sup>238</sup> U		C 2 2 L	11.9 ± 7.0	<sup>242m</sup> Am/ <sup>238</sup> U			12.3 ± 7.0
<sup>243</sup> Am/ <sup>238</sup> U	JCLL-	э.т.т Г	-0.1 ± 4.1	<sup>243</sup> Am/ <sup>238</sup> U	JEL	г-э.э 🗌	-2.6 ± 4.1	<sup>243</sup> Am/ <sup>238</sup> U	JCLL-	4.010 L	-0.4 ± 4.1
<sup>243</sup> Cm/ <sup>238</sup> U			-5.0 ± 15.0	<sup>243</sup> Cm/ <sup>238</sup> U			24.6 ± 15.0	<sup>243</sup> Cm/ <sup>238</sup> U			23.4 ± 15.0
<sup>244</sup> Cm/ <sup>238</sup> U	•	•	1.0 ± 5.6	<sup>244</sup> Cm/ <sup>238</sup> U	•	•	11.8 ± 5.6	<sup>244</sup> Cm/ <sup>238</sup> U	•	•	14.2 ± 5.6
<sup>245</sup> Cm/ <sup>238</sup> U	•	•	3.5 ± 7.5	<sup>245</sup> Cm/ <sup>238</sup> U	•	•	25.3 ± 7.5	<sup>245</sup> Cm/ <sup>238</sup> U	•	•	28.0 ± 7.5
<sup>246</sup> Cm/ <sup>238</sup> U	•	•	-15.2 ± 8.2	<sup>246</sup> Cm/ <sup>238</sup> U	•	•	-1.3 ± 8.2	<sup>246</sup> Cm/ <sup>238</sup> U	•	•	0.5 ± 8.2
<sup>247</sup> Cm/ <sup>238</sup> U	•	•	1.8 ± 29.7	<sup>247</sup> Cm/ <sup>238</sup> U	•	•	11.5 ± 29.7	<sup>247</sup> Cm/ <sup>238</sup> U	•	٠	13.5 ± 29.7
<sup>143</sup> Nd/ <sup>238</sup> U	-0.8 ± 0.6	-0.6 ± 0.6	-0.5 ± 0.5	<sup>143</sup> Nd/ <sup>238</sup> U	-0.1 ± 0.6	0.1 ± 0.6	0.2 ± 0.5	<sup>143</sup> Nd/ <sup>238</sup> U	-0.1 ± 0.6	0.1 ± 0.6	0.3 ± 0.5
<sup>144</sup> Nd/ <sup>238</sup> U	-1.3 ± 0.8	-1.5 ± 0.8	-1.6 ± 0.9	<sup>144</sup> Nd/ <sup>238</sup> U	-1.2 ± 0.8	-1.6 ± 0.8	-1.9 ± 0.9	<sup>144</sup> Nd/ <sup>238</sup> U	-1.1 ± 0.8	-1.6 ± 0.8	-1.8 ± 0.9
<sup>145</sup> Nd/ <sup>238</sup> U	0.0 ± 0.7	-0.1 ± 0.7	-0.5 ± 0.6	<sup>145</sup> Nd/ <sup>238</sup> U	0.3 ± 0.7	0.0 ± 0.7	-0.7 ± 0.6	<sup>145</sup> Nd/ <sup>238</sup> U	0.5 ± 0.7	0.4 ± 0.7	0.0 ± 0.6
<sup>146</sup> Nd/ <sup>238</sup> U	-0.3 ± 0.8	-0.4 ± 0.8	-0.1 ± 0.8	<sup>146</sup> Nd/ <sup>238</sup> U	0.6 ± 0.8	0.7 ± 0.8	1.1 ± 0.8	<sup>146</sup> Nd/ <sup>238</sup> U	0.3 ± 0.8	0.2 ± 0.8	0.3 ± 0.8
<sup>148</sup> Nd/ <sup>238</sup> U	0.5 ± 0.8	0.5 ± 0.7	0.6 ± 0.8	<sup>148</sup> Nd/ <sup>238</sup> U	1.5 ± 0.8	1.5 ± 0.7	1.6 ± 0.8	<sup>148</sup> Nd/ <sup>238</sup> U	1.0 ± 0.8	0.9 ± 0.7	1.0 ± 0.8
<sup>150</sup> Nd/ <sup>238</sup> U	-0.4 ± 0.9	-0.1 ± 0.8	$0.0 \pm 0.8$	<sup>150</sup> Nd/ <sup>238</sup> U	-0.1 ± 0.9	0.0 ± 0.8	0.1 ± 0.8	<sup>150</sup> Nd/ <sup>238</sup> U	-0.1 ± 0.9	0.1 ± 0.8	0.2 ± 0.8
Σ <sup>i</sup> Nd/ <sup>238</sup> U	0.0 ± 1.0	0.0 ± 1.0	0.0 ± 1.0	Σ <sup>i</sup> Nd/ <sup>238</sup> U	0.7 ± 1.0	0.6 ± 1.0	0.6 ± 1.0	Σ <sup>i</sup> Nd/ <sup>238</sup> U	0.5 ± 1.0	0.4 ± 1.0	0.4 ± 1.0
BU Cray. [GWjj/t]]	13.6	22.0	35.2	BU Cray. [GWjj/t]]	13.6	22.0	35.2	BU Cray. [GWjj/t]]	13.6	22.0	35.2

While C/E results are consistent with experimental uncertainties, they show different trends with burnup, suggesting that some cross sections should be revised: <sup>236</sup>U and <sup>239</sup>Pu radiative capture and <sup>238</sup>Pu production

#### **4.3 Commercial LWR applications (UPM)**

• UPM analyzed C/E for PWR Critical Boron Letdown Curve Almaraz II NPP – Cycle I (IAEA-TECDOC-815, 1995)



Modification Boron Let down (in ppm) - PWR Almaraz Cycle I

#### **Nuclear Data:**

Reference: ENDF/B-VII.1

Case JEFF-4T3\_U8J4T2

- XS/JEFF-4T3 + U8/JEFF-4T2
- D TSL /JEFF-4T3
- DD/JEFF-3.3
- □ FY\_U5\_PU9/JEFF-4/CON

Full core simulations expensive to be used in ND validation

Many compensating effects, no clean benchmarks

But able to identify general trends due to ND



#### 5.1. SINBAD benchmarks for validation of recent Fe evaluations (ENDF/B-VIII.0, JEFF-3.3 and FENDL-3.2)

Benchmark / quality	Additional information needed on:
ASPIS Iron-88 ~ ♦♦♦ Analyses by UKAEA (I.Kodeli)	<ul> <li>Review: new MCNP model. Additional information needed on:</li> <li>detectors arrangement (e.g. stacking)</li> <li>gaps between the slabs</li> <li>absolute calibration of neutron source &amp; dilution factor</li> <li>effect of the cave walls</li> </ul>
ORNL PCA Pool Critical Assembly - PV Benchmark (1980) Analyses by NRG (S.v.d. Marck)	<ul> <li>approximate modelling of neutron source (material test reactor (MTR) with a 93% <sup>235</sup>U fuel elements)</li> <li>SINBAD quality evaluations to be performed</li> </ul>
ASPIS PCA REPLICA - Winfrith Water/Steel ♦♦♦ Analyses by UKAEA (I.Kodeli)	<ul> <li>Supplementary information received from David Hanlon (Jacobs) on (available from WPEC SG47 Githab):</li> <li>geometrical arrangement of the fission plate and ASPIS cave;</li> <li>geometry and material of the detectors;</li> <li>measurement arrangement and background contribution</li> <li>availability of <sup>235</sup>U fission chamber measurements</li> </ul>
CIAE Iron slab 14 MeV benchmark Analyses by UKAEA (I.Kodeli)	<ul> <li>Ongoing SINBAD evaluation (presented at WPEC SG47)</li> <li>TOA neutron spectra measured from 5, 10 and 15 cm Fe slabs at 60<sup>o</sup> and 120<sup>o</sup> (~2016)</li> </ul>



C/E for S(n,p) and Al(n,α) using ASPIS-Fe88, PCA & PCA Replica

Sensitivity profiles to <sup>56</sup>Fe(n,n') in deepest positions for PCA, PCA Replica vs. ASPIS Fe88

SANDA Meeting, 5 February 2024

#### **5.2. KFK-1977** γ-ray leakage benchmark

• New SINBAD evaluation by Stanislav Simakov: KFK-1977 measured gamma from bare 252Cf(s.f.) source and from Ø25, 30 and 35 cm Fe spheres was prepared within WPEC SG47





#### KFK set-up:



KFK vs. IPPE: γ-ray leakage spectra from Fe Ø30cm with Cf-source



#### **5.3. TOF Shielding Benchmarks in SINBAD**

- FNS TOP (17 cases x 5 angles)
- Oktavian (15 cases)

ENS-TOF/50.0 CM(R)\*60.0 CM(Z)-FE CYL.

• MCNP6 shielding suite (14 cases)





FNS/TOF results

SANDA Meeting, 5 February 2024



- Significant number of sets of reactor physics & shielding benchmarks, as planned
  - Extensive use of JEFF-3.3 and JEFF-4Tx for C/E estimates and trends identified
  - Deliverable structure already shared with all contributors (January 2024)
- Pending to send a draft so that contributors can include additional updated results/analysis
- $\checkmark$ 
  - Estimated date to send a 1<sup>st</sup> draft to contributors: March 2024
- Estimated date for completion: April 2024